



Simulation of Ares Scale Model Acoustic Test Overpressure Transients Using Computational Fluid Dynamics

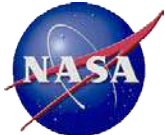
Acoustical Society of America Meeting

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Gabriel Putnam

ESTS Group/All Points Logistics/ER42/MSFC



Outline



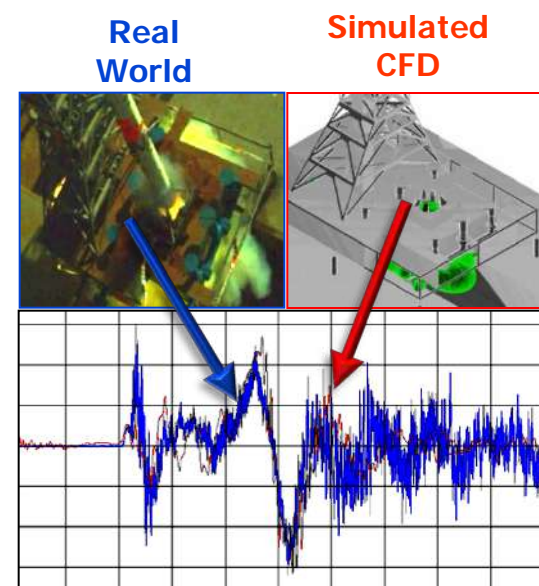
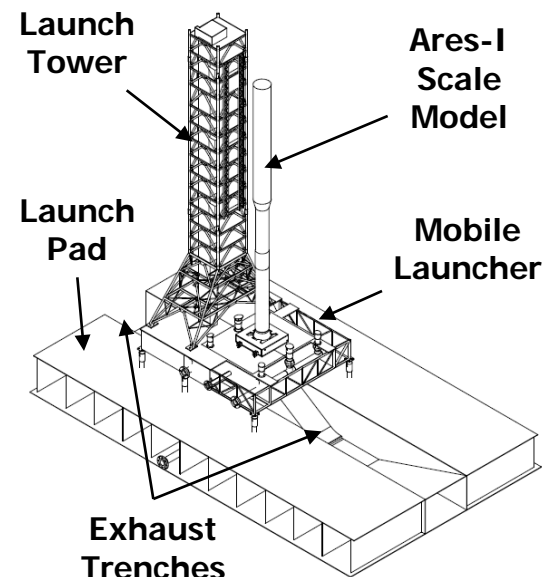
- Introduction
 - Overview of the Ares Scale Model Acoustic Test (ASMAT)
 - Simulation goal and procedure
- Case Progression
 - Initial Attempt at Elevation 0' (Pathfinder)
 - Ignition Transient and Throat Plug Release
 - Model Refinement
- Conclusions / Future Work



Introduction : ASMAT Overview



- Ares Scale Model Acoustic Test
 - Tests of 5% scale model of Ares I vehicle
 - Addressed vibration / acoustic risks from Constellation Program.
- Physical Test Setup
 - Scale model powered by Rocket Assisted Take-Off (RATO) motor
 - Vehicle at point of, or just after, lift-off
 - Stationary in space during firing
 - 100+ pressure transducers on the launch structure and vehicle (locations later)
- Simulation Interest
 - Well documented set of high fidelity measurements for CFD validation
 - Demonstration of CFD capability for IOP prediction





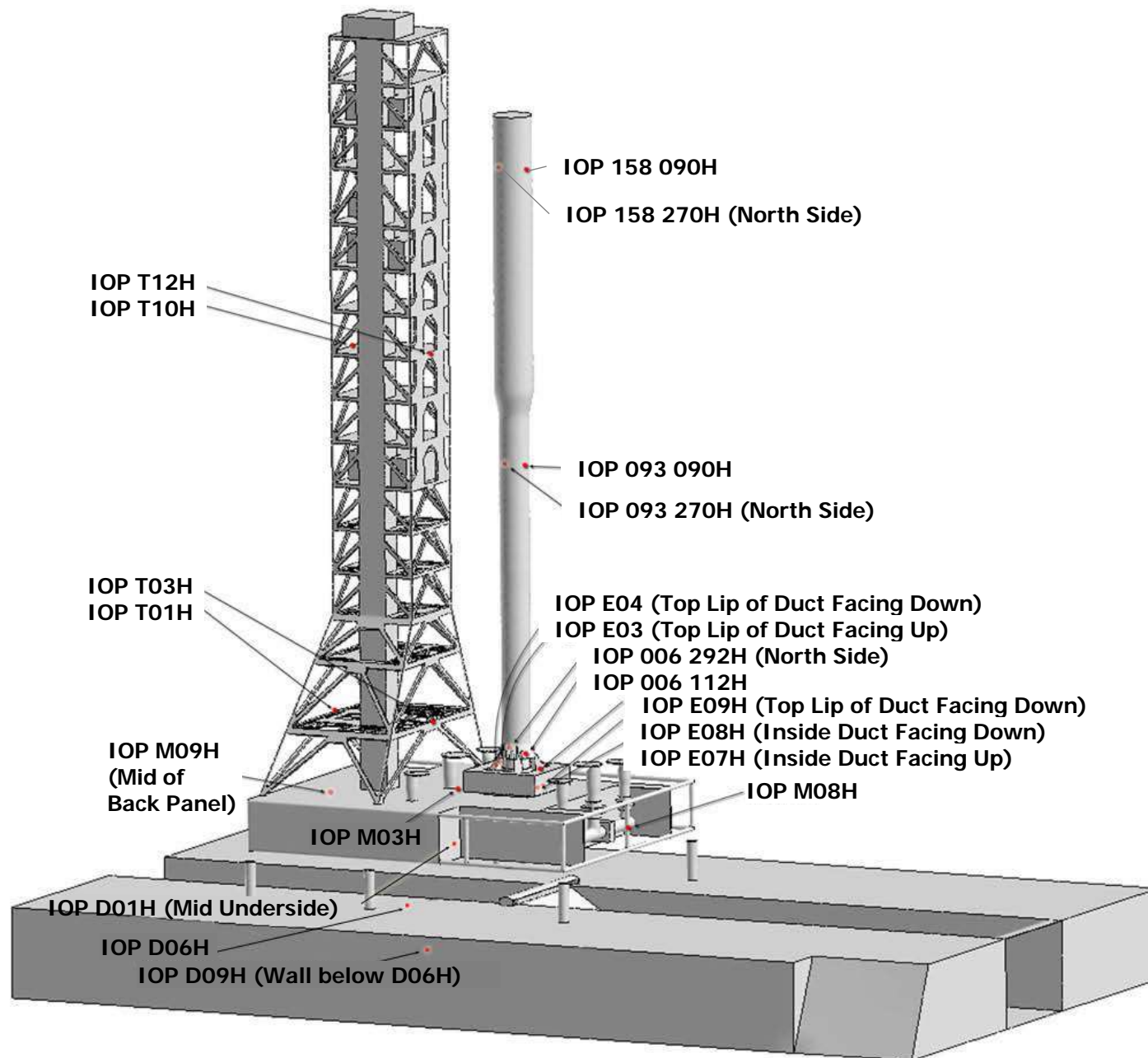
Introduction : Goals and Procedure



- Simulate transient startup of the ASMAT tests
- Evaluate pressure / temporal / spectral accuracy of code.
- Predict the Ignition Over-Pressure (IOP) on a launch pad
- General Procedure
 - Execute CFD simulations of the first 0.1 seconds of the tests
 - Ignition and throat plug loss
 - Ramp up to full power
 - Overpressure wave propagation
 - Simulation times of roughly 1 week using 1000 CPUs at Pleiades
 - Compare simulation data to pressure transducer data
 - Range of sensors across the vehicle, trench, pad, and tower
 - Specific sensors and locations on next page
 - Compare Pressure vs Time and SPL vs Freq
 - Compare wave / flow propagation to available imagery
 - Visible / IR wave cameras



Sensors Used for Comparison

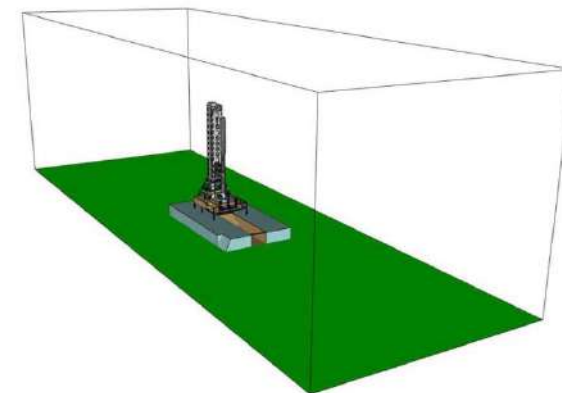
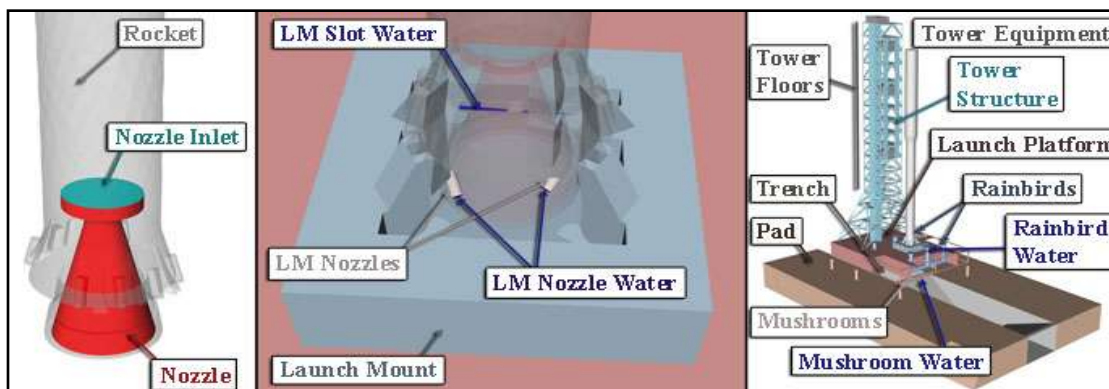
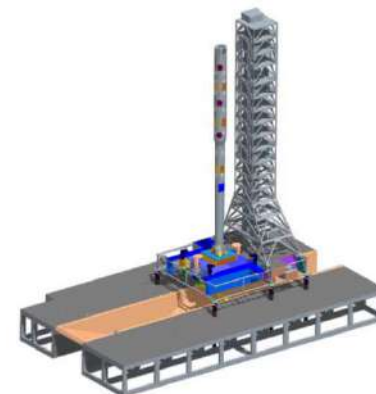




Case Progression : Pathfinder : Setup



- Obtained CAD model of ASMAT structure from ET50
 - Overly detailed (two upper right images)
 - Visited pad and took lots of pictures to understand important features
- Created a simplified version of structure
- Used ANSA to divide model into components, create mesh, and place structure within a computational domain (bottom images)

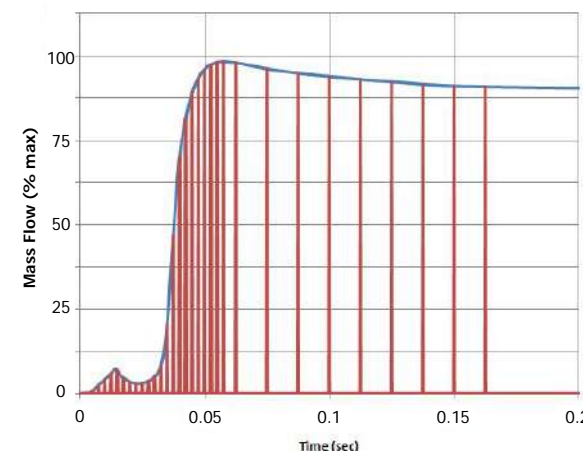
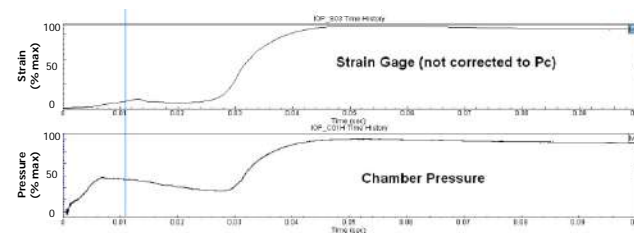




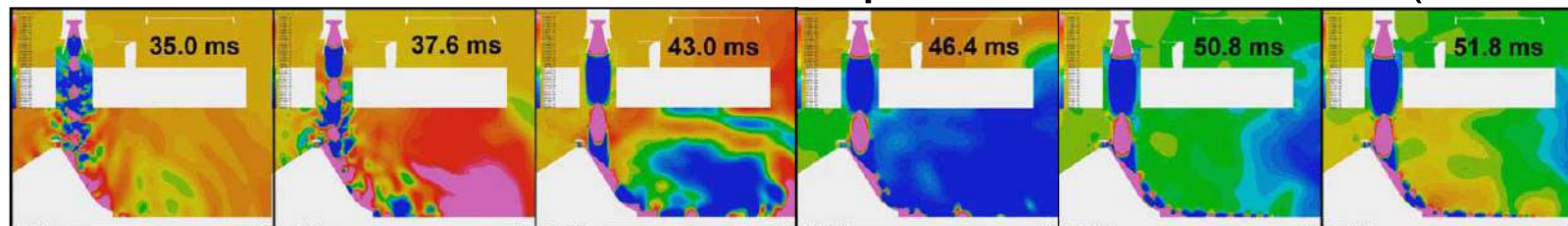
Case Progression : Pathfinder : Setup



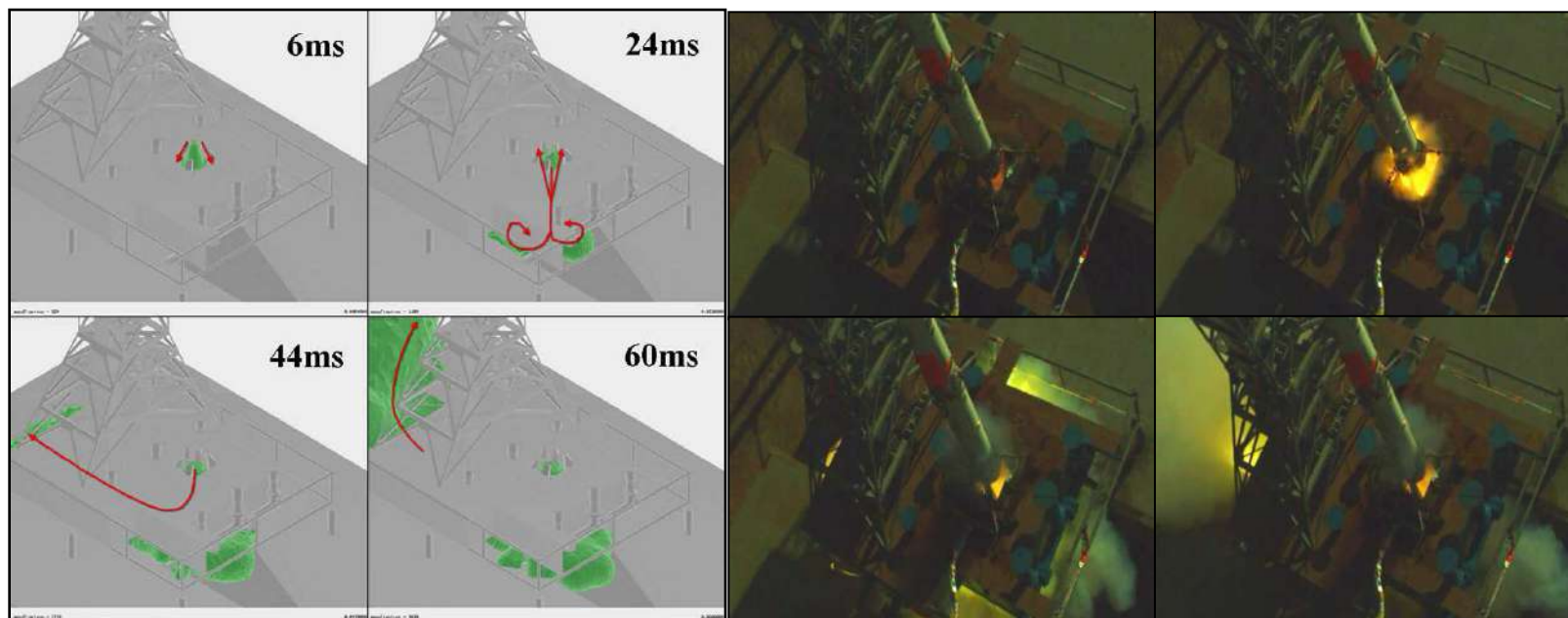
- Target comparison case – IOP3
 - Dry launch pad
 - 0' elevation, no drift
- Creating a mass flow profile
 - Started with pressure trace
 - Initially from from chamber pressure
 - Ignition corrected using casing strain gages
 - Assumed mass flow proportional to pressure
 - Scale max mass flow to match RATO specs
 - Obtained from ESTSG-FY10-02462
 - Manufacturer supplied maximum
 - Took targeted samples of profile
 - Allowed CHEM to interpolate between them



- Qualitative visualization of overpressure formation (video)



- Qualitative comparison of effluent to imagery (video)

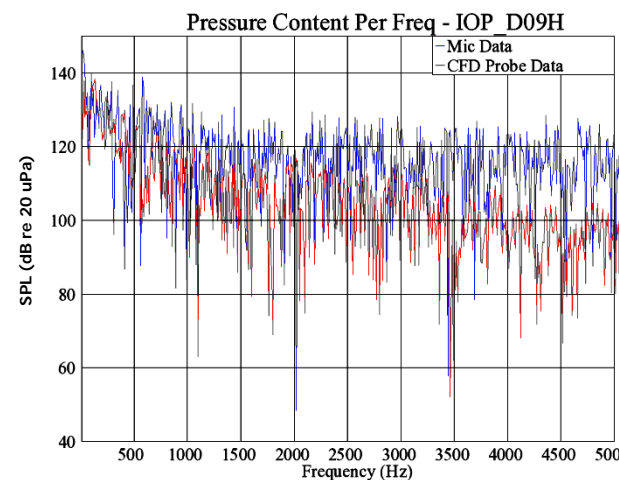
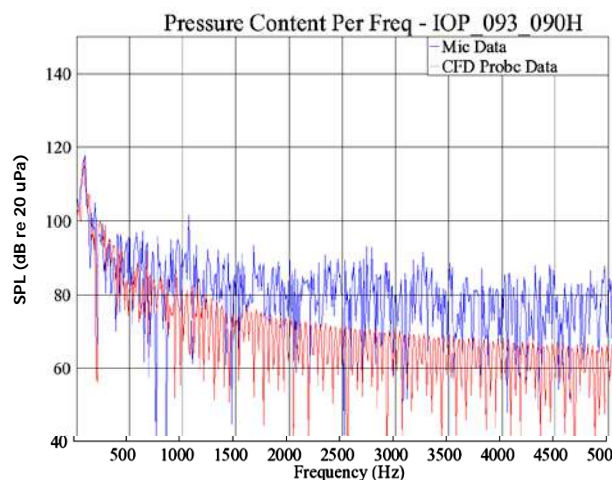
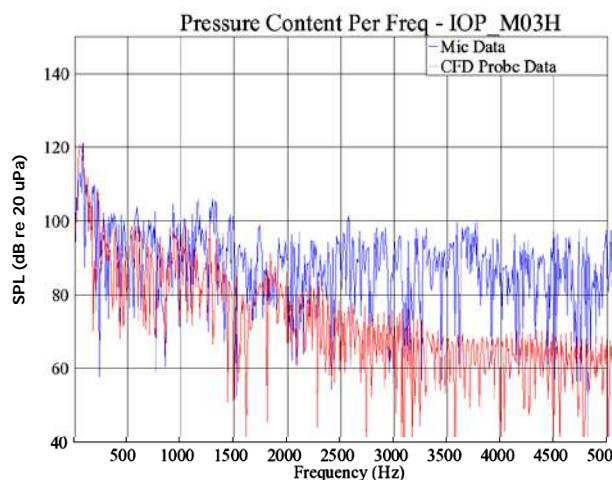
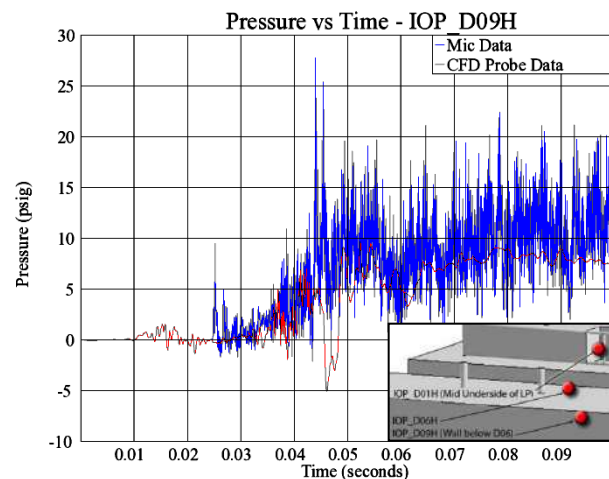
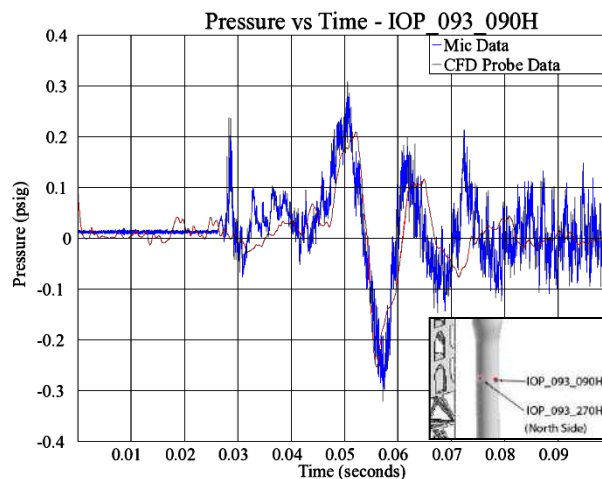
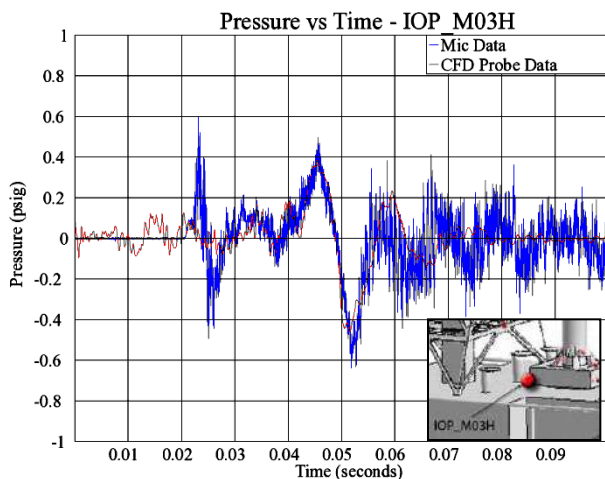




Case Progression : Pathfinder : Results



- Quantitative comparison of time and freq domain signals



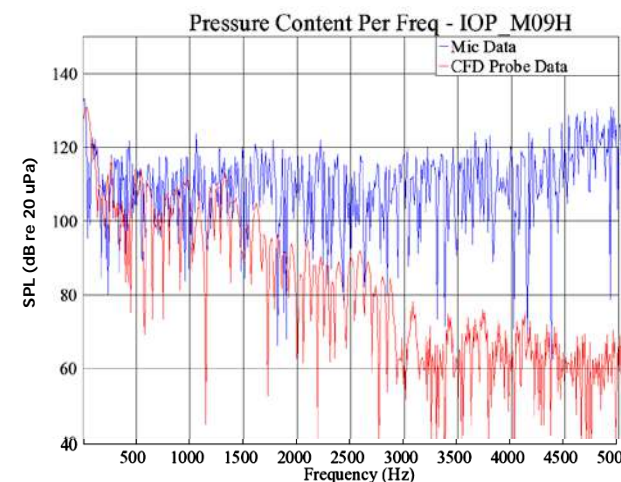
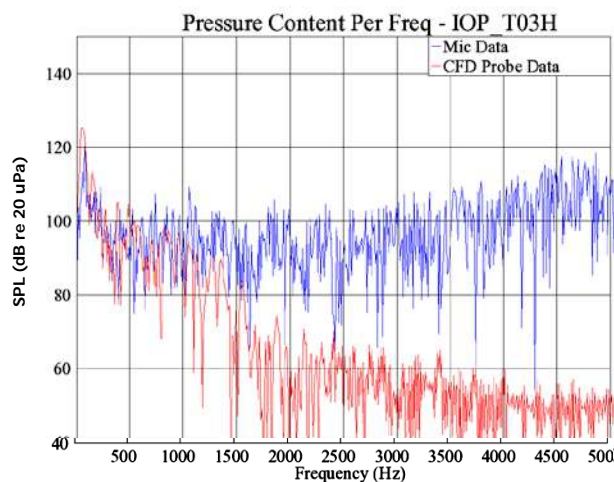
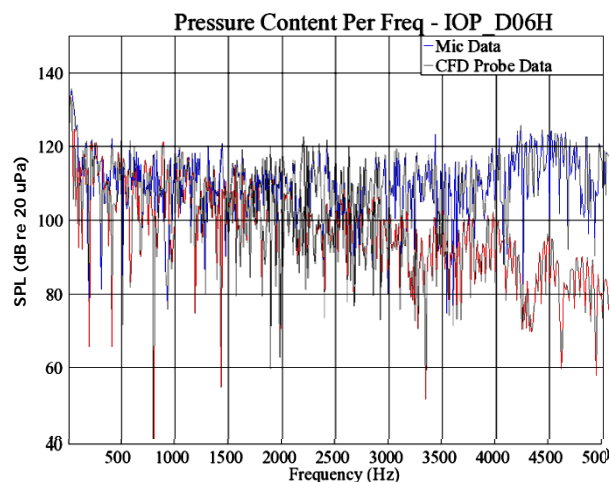
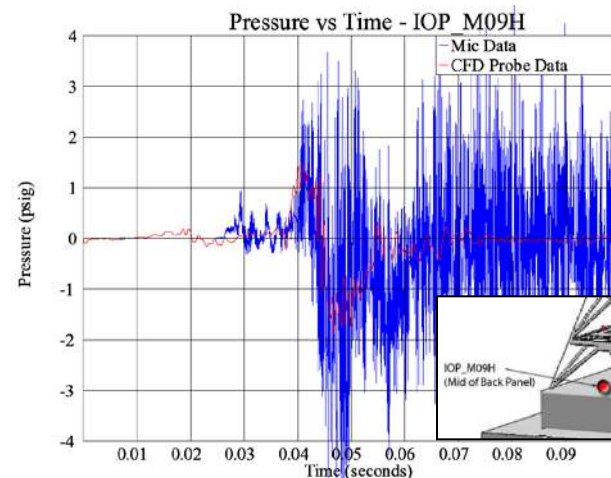
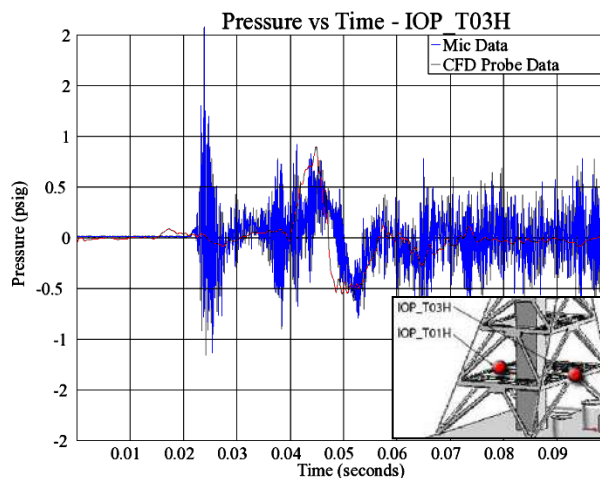
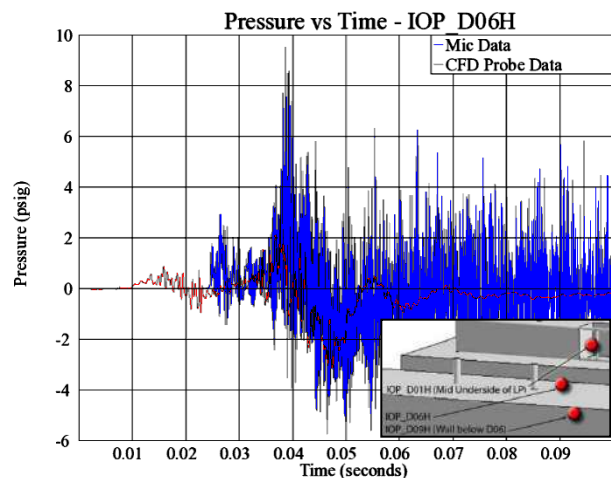
BLUE is test data, RED is CFD data



Case Progression : Pathfinder : Results

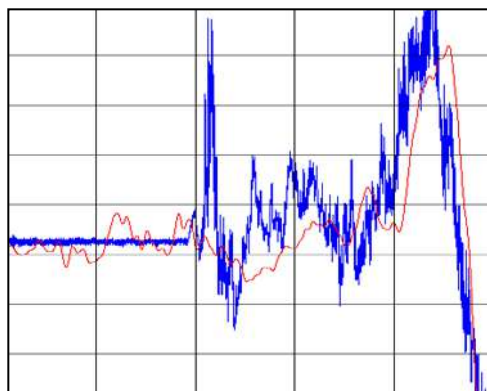
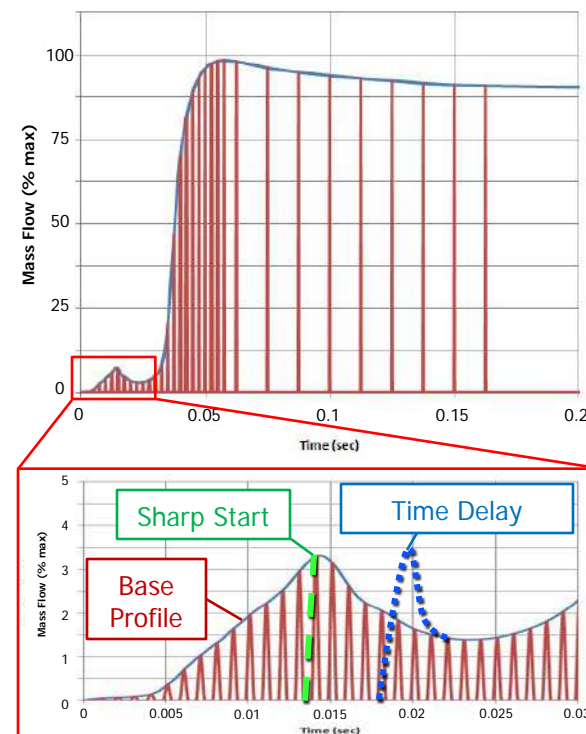


- Quantitative comparison of time and freq domain signals

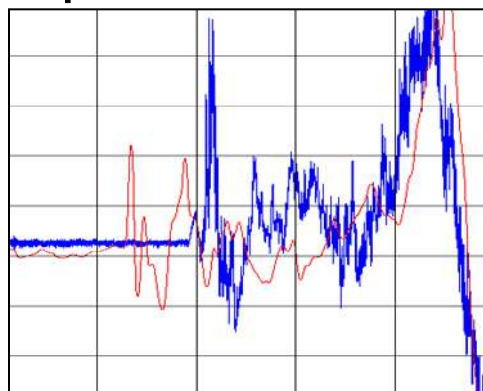


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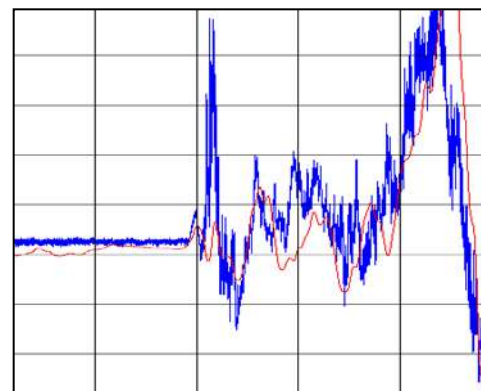
- First profile based on pressure rise rate
 - Scaled from pressure rise rate
 - Throat plug loss not taken into account
- Changed profile in the ignition region
 - First used sharp start at pressure peak to simulate throat plug loss
 - Captured sharp spike at flow start
 - Timing mismatch with measured signals
 - Moved pressure peak to match time delay.
- Effect on simulated pressure



Original Flow Profile

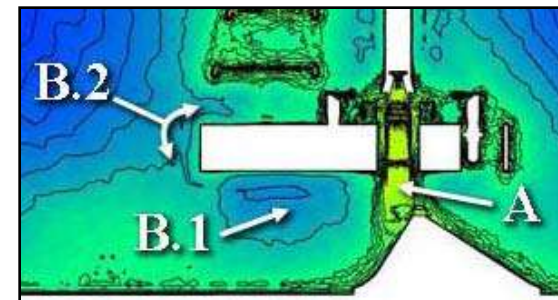


With Sharp Start

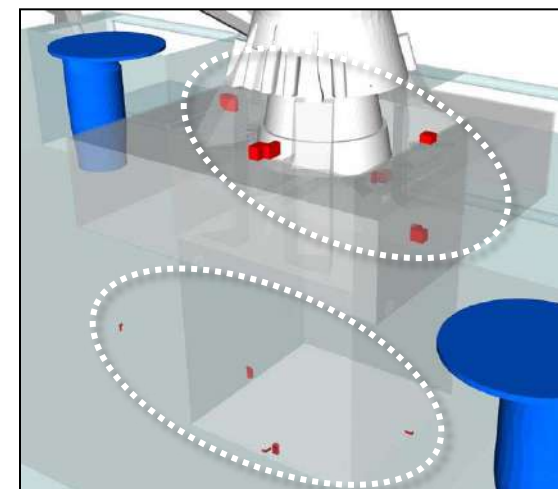


Time Delayed Sharp Start

- Issues with prior simulations and meshes
 - Poor mesh quality below the deck and tower
 - Lack of proper microphone mounts



- What was changed in the refinement
 - Fixed all low resolution areas
 - Added microphone mounts for all mics used
 - Overall resolution increase in trench and near rocket skin
 - Included time-delayed, sharp start for ignition and throat plug loss mass flow

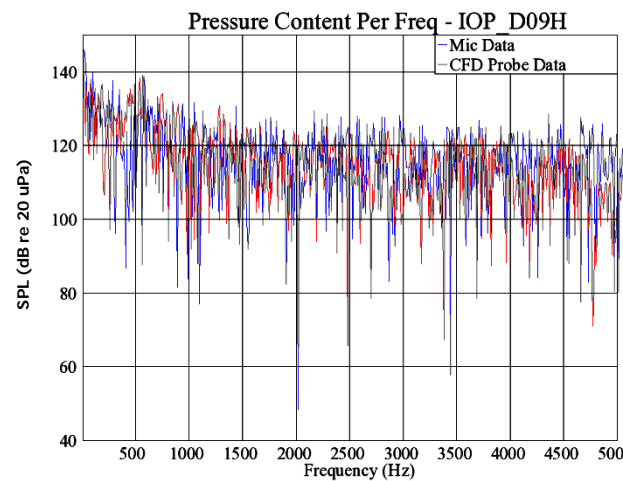
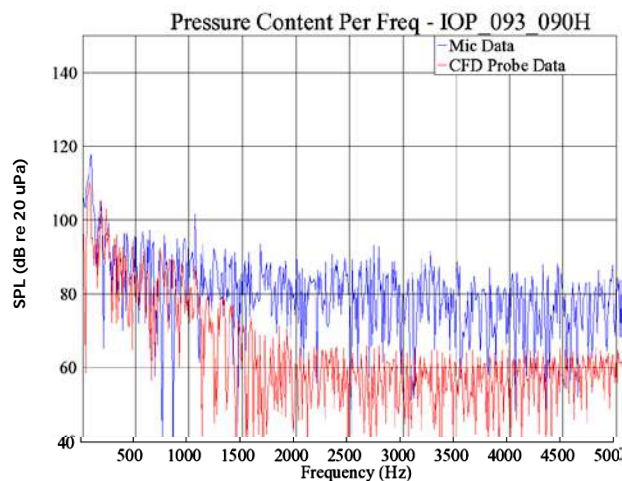
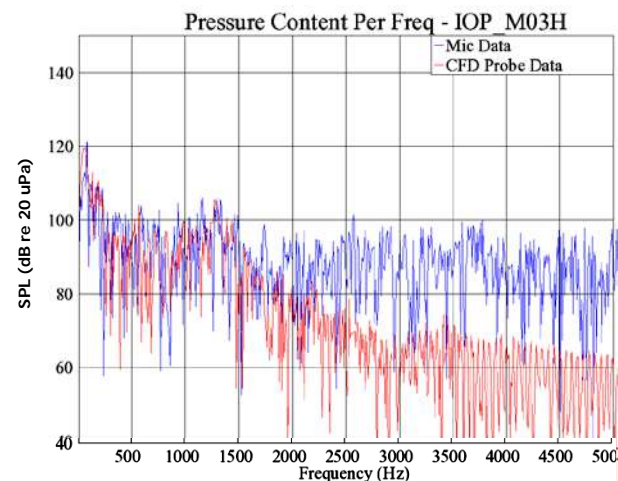
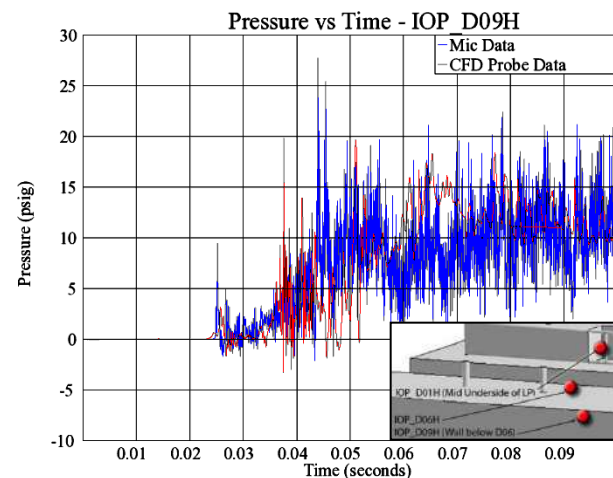
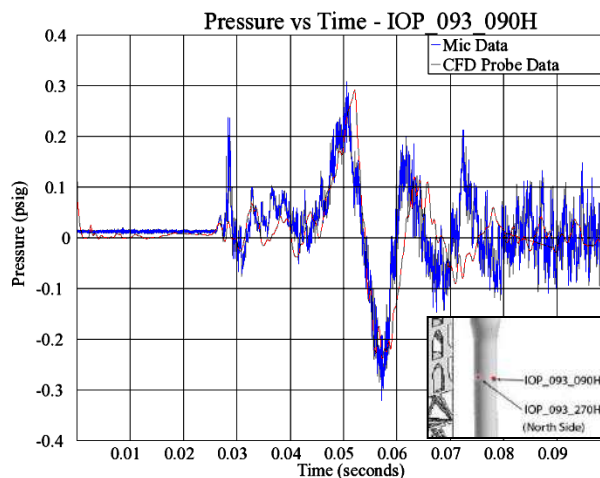
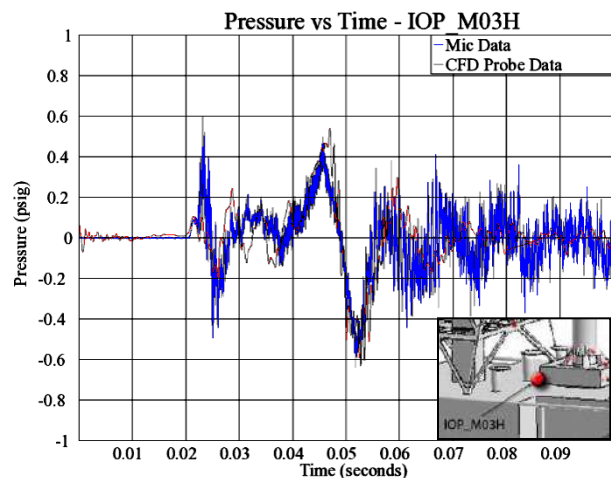




Case Progression : Pathfinder Refined : Results



- Quantitative comparison of time and freq domain signals



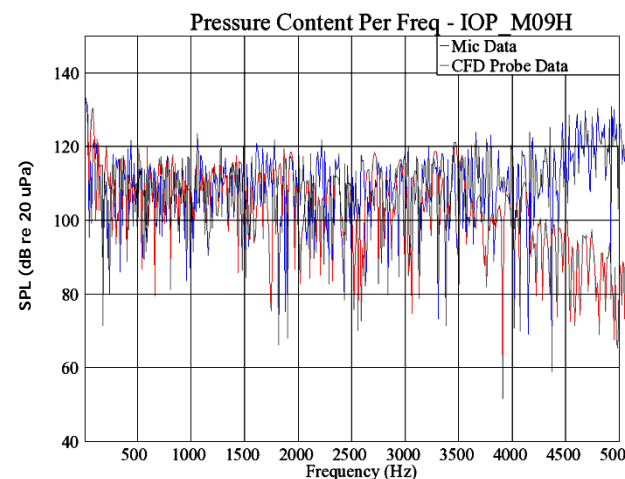
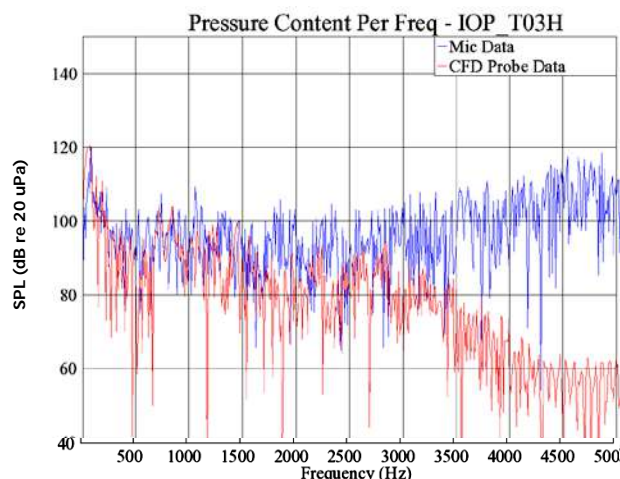
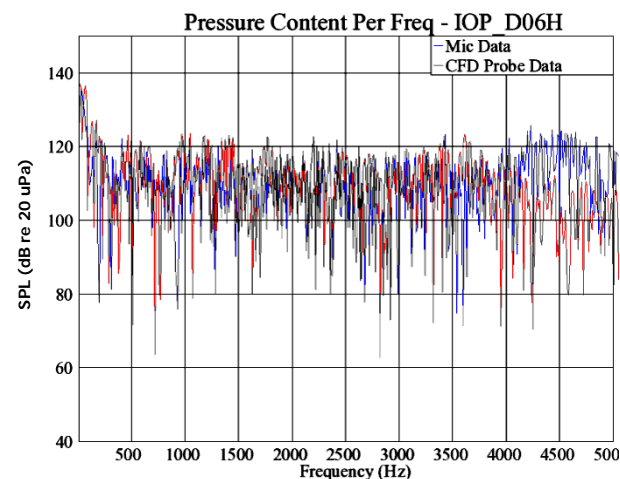
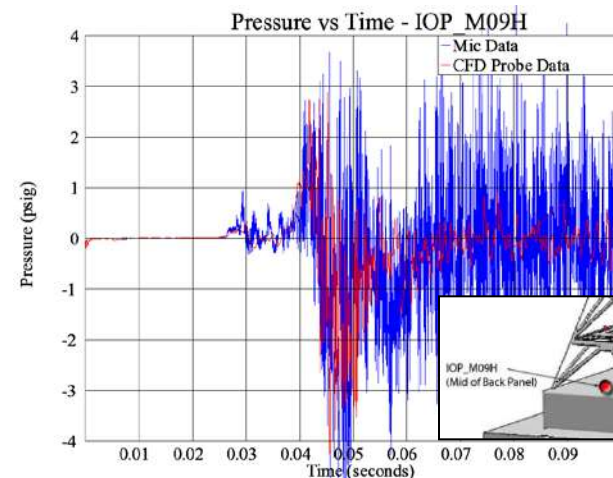
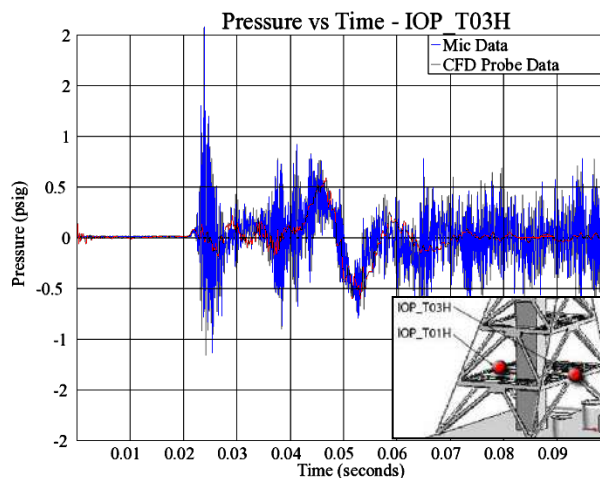
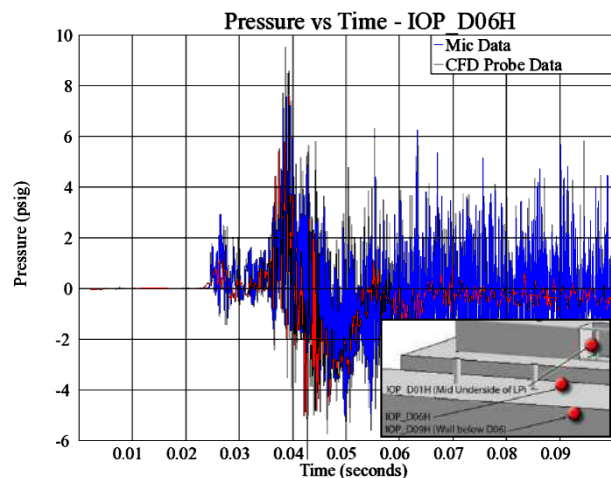
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Case Progression : Pathfinder Refined : Results



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Conclusions / Forward Work



- Overpressure can be simulated in a dry state
 - Major pressure peak amplitudes captured with 5-10% error
 - Major pressure peak timings captured similarly well
- Unresolved Issues with timing and water
 - Timing of ignition transient and throat plug loss that still needs to be explained, although time delay appears to match well
 - Large scale water use currently fails when water is compressed against solid walls and limits applications for in-trench deluge
 - Short-term – Implement method to automatically remove overly dense liquids near walls
 - Long-term - Implement shallow liquid pooling models for near-wall liquid collection
- Forward work
 - Freq content of signals currently captured out to 1500-3000 Hz depending on sensor and transmission path
 - Attempt simulation of quasi-steady acoustics



Backup



Backup Slides



CFD Parameters Used



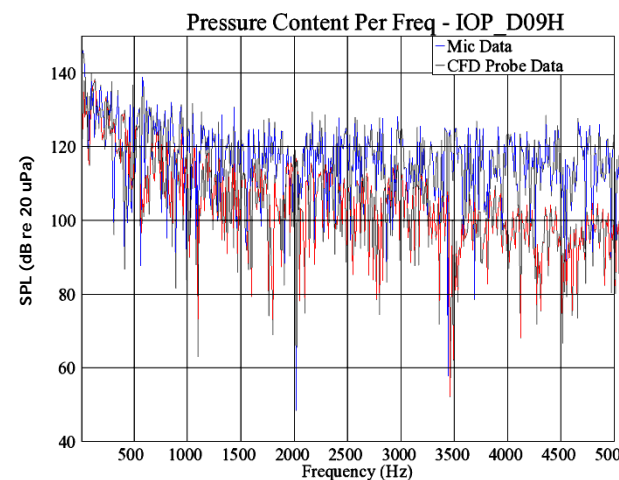
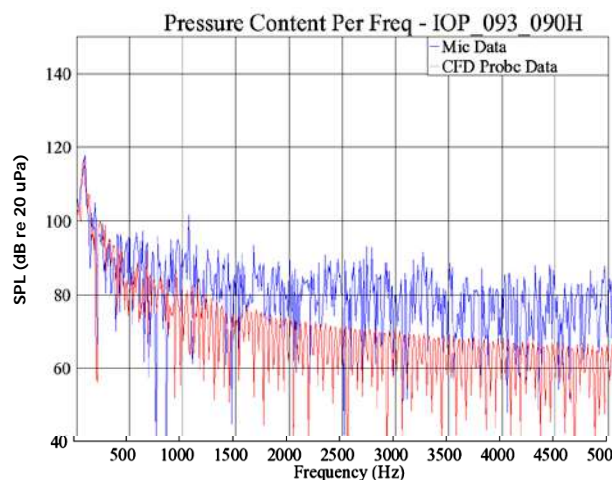
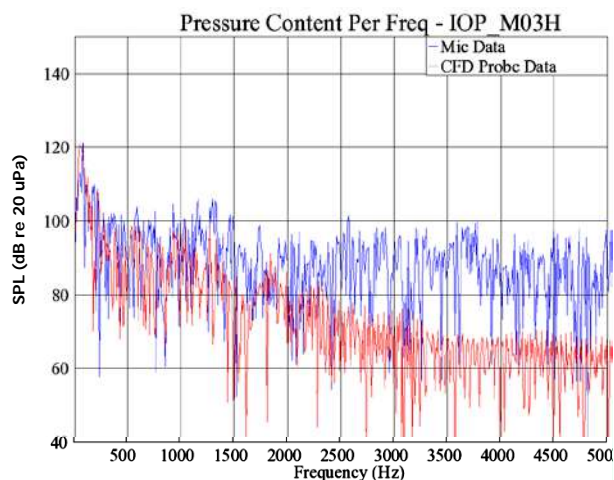
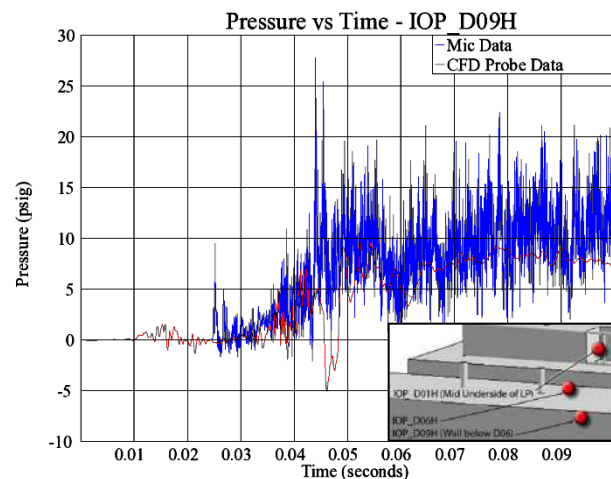
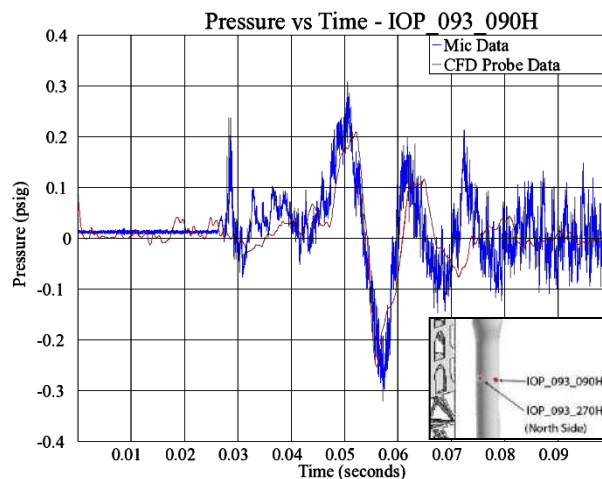
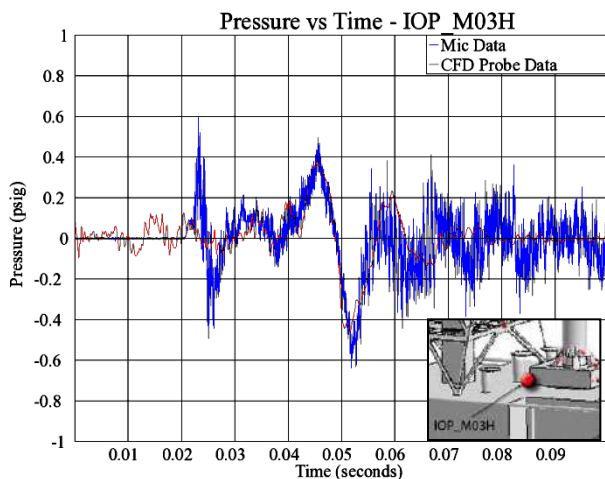
- **Gas Chemistry:**
 - Frozen chemistry, mixed heavy gas model
 - Air, and RSRM effluent (a heavy gas, RATO motor, effluent approximation) as the working fluids.
- **Transport Model:**
 - Sutherland model for viscosity and thermal conductivity using properties for air.
- **Diffusion Model:**
 - Laminar Schmidt
 - Simultaneous mass and momentum diffusion convection processes with Laminar Schmidt Number = 0.9
- **Turbulence Model and Method:**
 - Menter's Shear Stress Transport (SST) two equation eddy viscosity turbulence model with limiters and vorticity source term (SST-V)
 - Coupled with Nichols-Nelson Hybrid RANS/LES model (Multiscale turbulence model where eddy viscosity is a function of two turbulent length scales).
- **Time Integration:**
 - Time Accurate, 2e-5 sec timesteps.
 - 7 Gauss Seidel iterations
 - 7 Newton sub-Iterations
- **Fluid Linear Solver:**
 - Symmetric Gauss Seidel solver.
- **Inviscid Flux Treatment:**
 - Riemann solver using Roe scheme with HLLE (Harten-Lax-van Leer-Einfeldt) algorithm for strong shock s.
- **Flux Limiter:**
 - Venkatakrishnan (Second-order spatial accuracy gradient reconstruction limiter with threshold of acceptance for small variances.)



Case Progression : Pathfinder : Results



- Quantitative comparison of time and freq domain signals



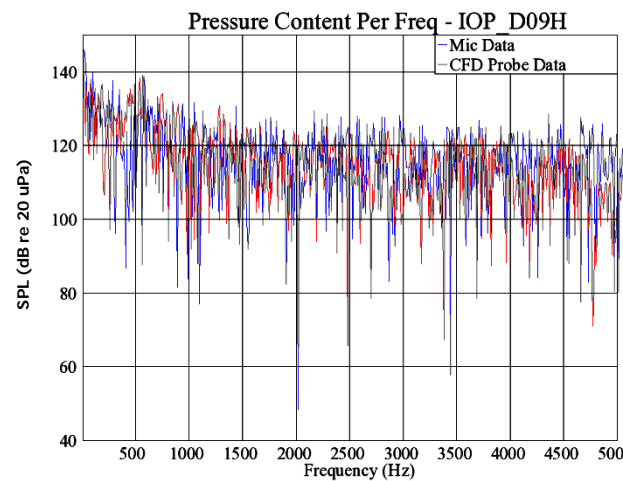
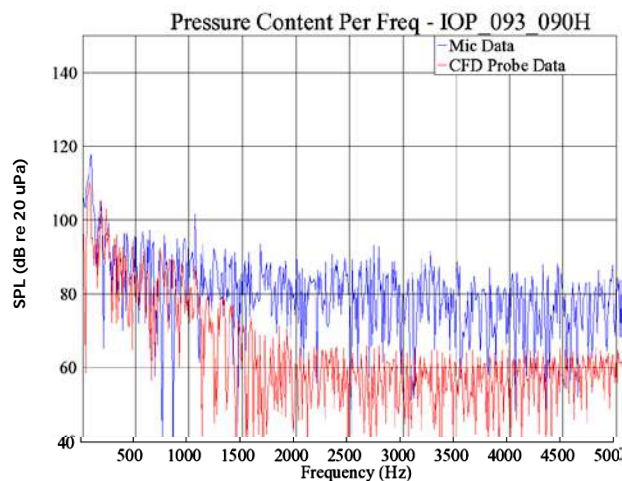
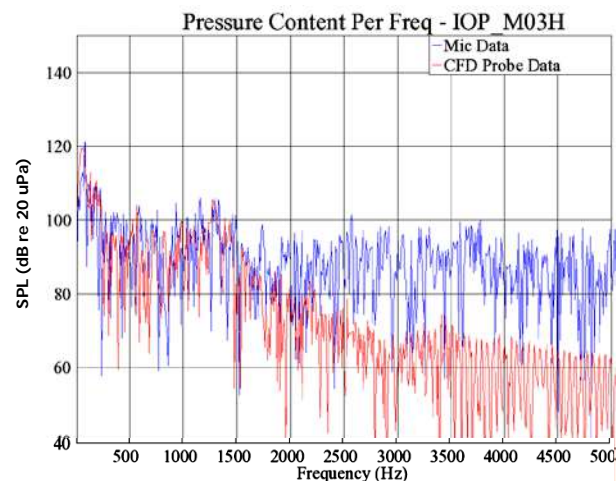
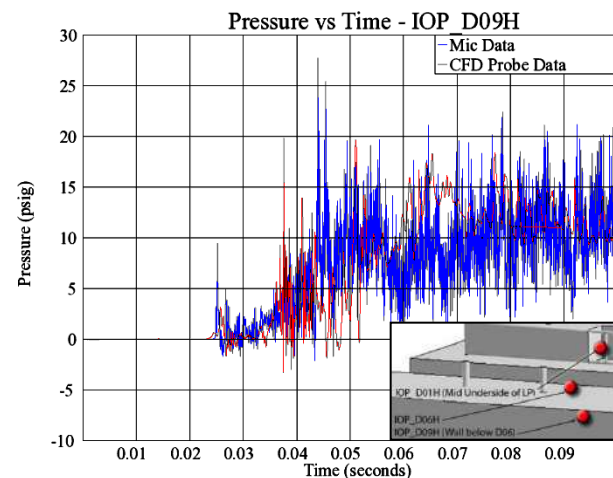
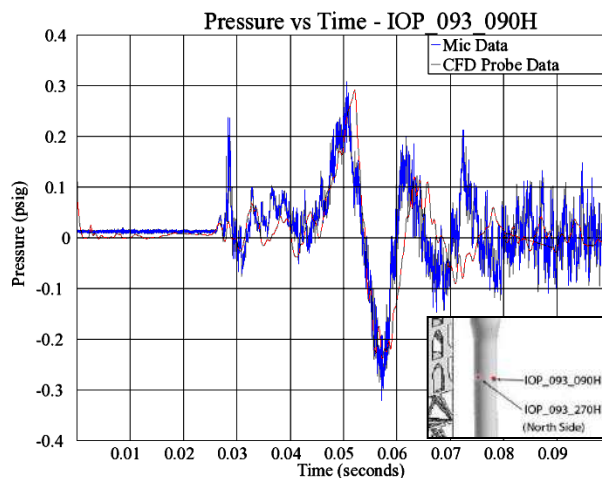
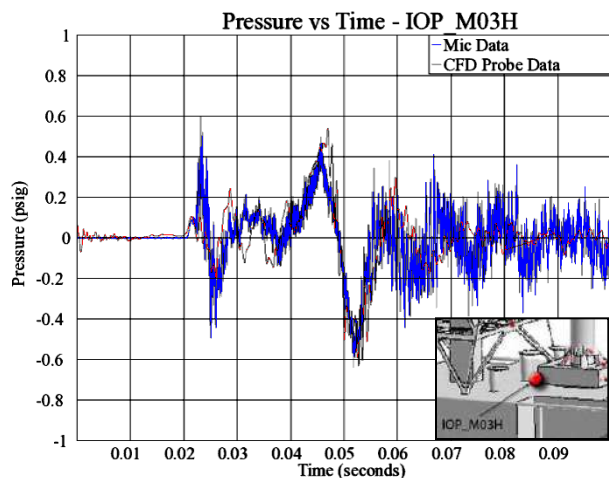
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Case Progression : Pathfinder Refined : Results



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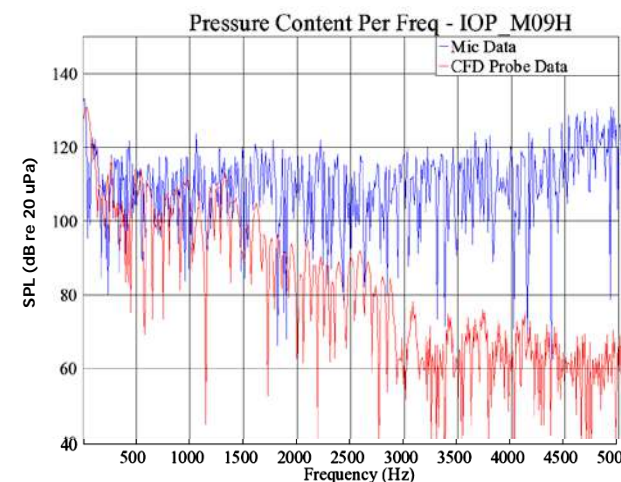
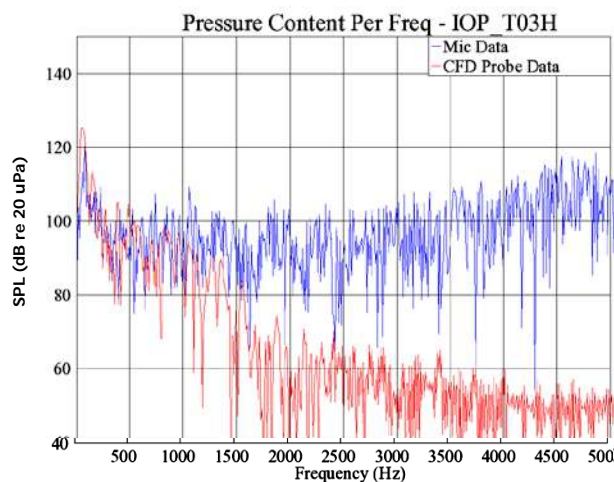
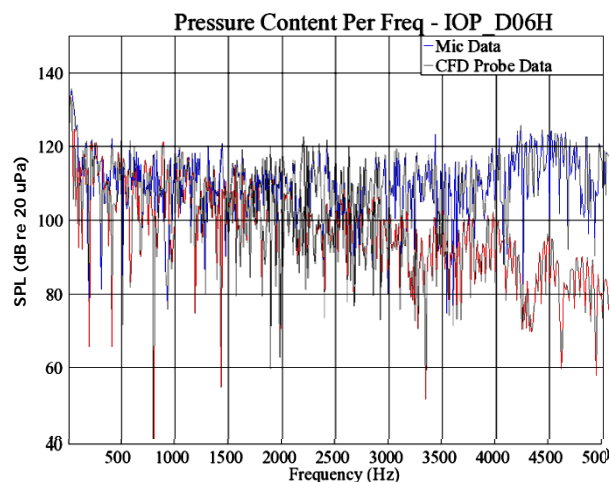
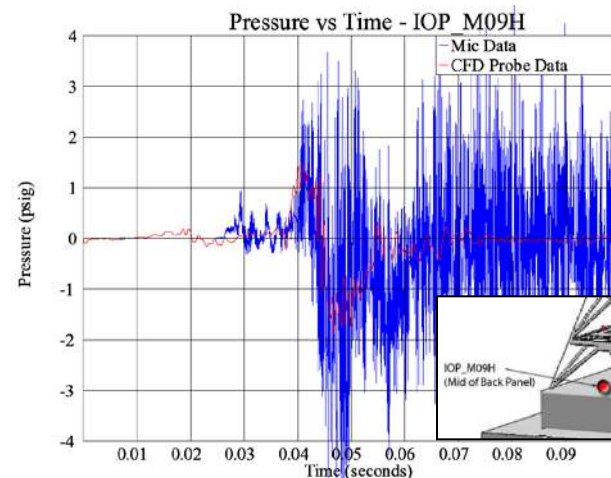
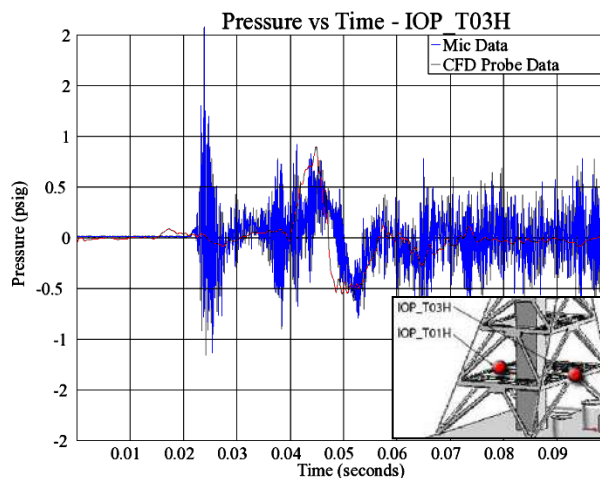
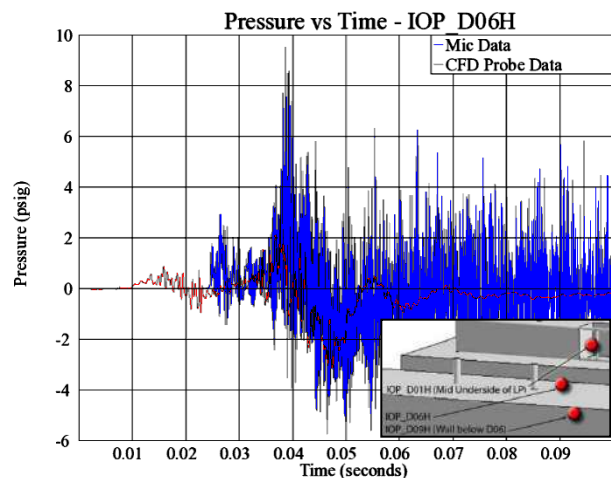
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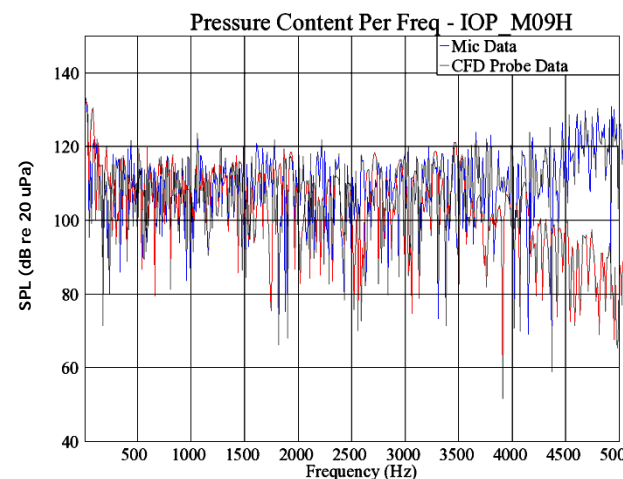
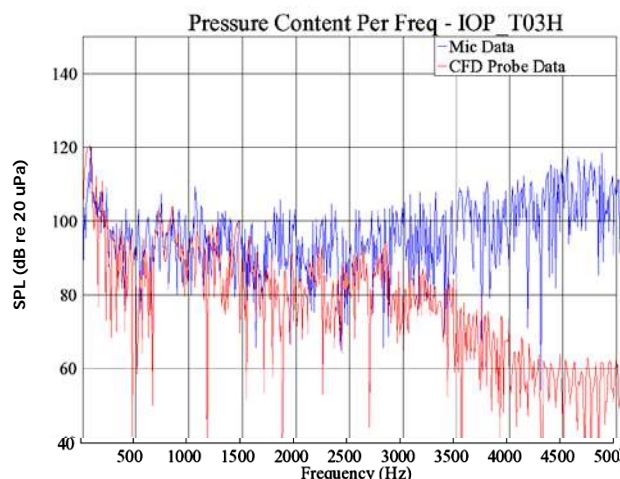
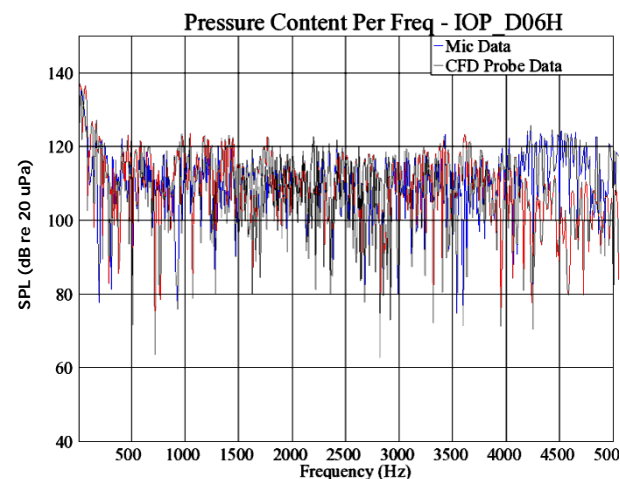
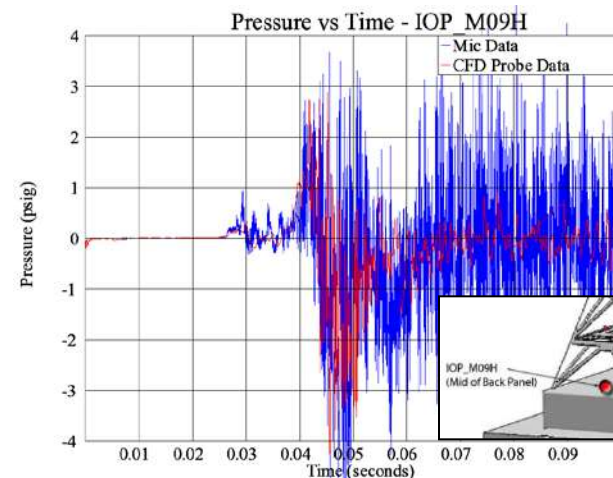
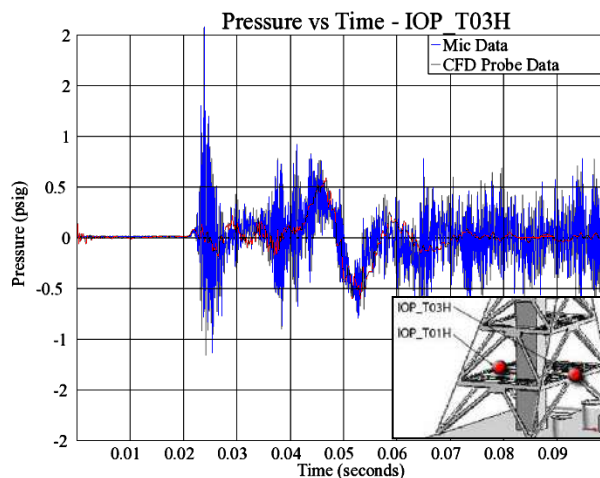
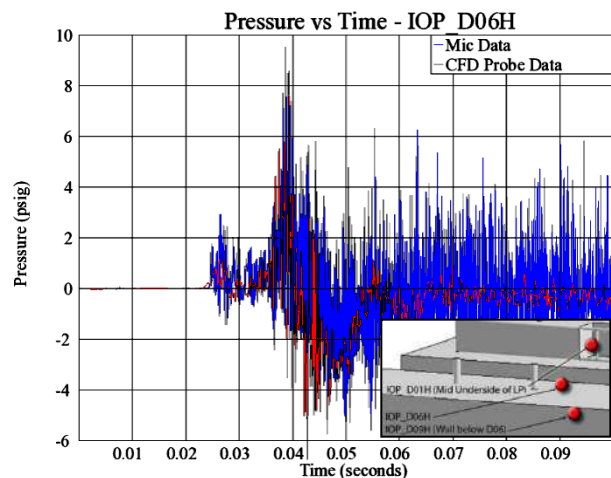
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